DOI: 10.5455/annalsmedres.2018.09.205

2019;26(1):106-12

# Long anatomical femoral stem reduces stress concentrations on femurs with lateral bowing deformity: A finite element analysis

Nihat Demirhan Demirkiran<sup>1</sup>, Mehmet Erduran<sup>2</sup>, Turan Cihan Dulgeroglu<sup>1</sup>

<sup>1</sup>Dumlupinar University, Kutahya Evliya Celebi Training and Research Hospital, Department of Orthopedics and Traumatology, Kutahya, Turkey <sup>2</sup>Dokuz Eylul University, Faculty of Medicine, Department of Orthopedics and Traumatology, Izmir, Turkey

Copyright © 2019 by authors and Annals of Medical Research Publishing Inc.

#### **Abstract**

Aim: Femoral morphology varies widely among different ages and sexes. Lateral bowing is a variance of the femur described in elderly females from Asian race. This bowing deformity is usually underestimated in patient evaluation and planning the most suitable treatment. In this study we aimed to evaluate the stress distribution around femoral prosthesis in femurs with lateral bowing deformity, using a finite-element (FE) method. The main objective of our study was to compare stress concentrations around five different stem models.

**Material and Methods:** A lateral femoral bowing deformity model was obtained from the post-operative CT data of a 69-year-old woman, using a software (3D-Slicer). Straight and anatomical femoral stem models with different lengths are designed on the model of von Mises stress concentrations of five different stem models are evaluated.

**Results:** The long anatomic stem did not lead to excessive stress concentrations on any area of the femur and a uniform stress distribution was obtained. The maximum von Mises stress for long anatomical stem (29,197 MPa) was lower than any other model. Highest stress concentrations were observed in medium straight stems (43,147 MPa).

**Conclusion:** For patients with a lateral bowing deformity, longer anatomical femoral stems may overcome the excessive stress shielding, providing stress distribution over a wider region of the femur.

Keywords: Femoral Lateral Bowing; Finite Element; Anatomical Stem; Hip Arthroplasty.

### INTRODUCTION

Total hip arthroplasty (THA) is one of the most common elective surgeries performed in older adults. As life expectancy in developed nations continues to increase; the ratio of the population older than 65 years old also rises, leading to more frequently performed THA surgeries. It is estimated that approximately 1-3% of the population older than 65 years will undergo THA at some point, with an average age of 66 (1). When the epidemiology of both primary and revision total hip replacement in the U.S. Medicare population is evaluated the rates of THA procedures were found to be higher among women than men (2). The number of revision THAs is also expected to increase significantly secondary to both the increasing life expectancy and the increasing number of primary THAs (3). As a result the incidence of periprosthetic fractures are

expected to rise; especially after revision surgeries (4-6).

The geometry and size of femoral stem is an important factor which affects the pattern of stress transferred to the femur. It has been known that a precise fit of the femoral stem in the femur minimizes stress shielding and for this purpose custom made implant designs have been suggested (7), owing to the fact that femoral structure and morphology varies widely among different ages and sexes (8).

Lateral bowing is a morphologic variance of the femur especially in elderly females from Asian race (9). During our clinical practice, we also have encountered a remarkable number of such patients in our institution. However to the best of our knowledge, there are no studies about the prevalence or biomechanical properties of this deformity, On the other hand, this bowing deformity is usually

Received: 26.09.2018 Accepted: 23.10.2018 Available online: 05.11.2018

Corresponding Author: Nihat Demirkinan Demirkiran, Dumlupinar University, Kutahya Evliya Celebi Training and Research Hospital, Department of Orthopedics and Traumatology, Kutahya, E-mail: drdemirhandemirkiran@gmail.com

underestimated in evaluation and treatment planning; for instance, anterior bowing of the femur has been taken into account during the design of long-stemmed prosthesis, however lateral bowing deformity is neglected. Furthermore, the effect of longer femoral stems on femurs with lateral bowing has not been studied before.

Therefore, we performed this study using a finite-element (FE) method. The research question of our study was 'what is the optimal length and curvature of the femoral stem to reduce stress shielding over femurs with lateral bowing deformity?' Our hypothesis was longer stems with anatomical curves on both sagittal and coronal planes would achieve a uniform stress distribution. We aimed to evaluate and compare the stress concentrations around five different stem models (short/medium/long straight and medium/long anatomical) in femurs with lateral bowing deformity.

Independent variables of our study was the length and shape of femoral stems. Dependent variables consisted of von Mises stress values caused by these different stem models.

#### **Geometrical Definitions**

The CT-based finite element method is used to evaluate the effect of stem length and stem geometry on patients with bowing deformity in the coronal plane. A CT data of lateral femoral bowing deformity were obtained from the postoperative CT of a 69-year-old woman, who had undergone revision hip arthroplasty using a 17mm X 150mm sized straight femoral stem (Arcos® Modular Femoral Revision System, Biomet Orthopedics, LLC, Warsaw, Indiana USA). The implant applied to this patient ended nearly on the apex of lateral bowing deformity (intersection of two femoral axes) and this data was used for creating the middle length straight stem model (Figure 1a). To compare different stem size effects accurately, implant geometry was simplified with some measurements (head diameter, neck-shaft angle, stem length and diameter) manually and remodeled. 3D bone geometries were obtained using free and open-source software 3D-Slicer (10) and all parts were segmented manually. Cortical and cancellous bone were modelled as separate sections. The femur was positioned with the center of the implant head coinciding with the origin of the global reference system and the x, y and z axes defined according to HIP 98 (11) (Figure 1b). In addition, lateral bowing deformity angle measured with an intersecting proximal and distal femoral axis (3 points: lower edge of the lesser trochanter, middle, and 100 mm proximal to the distal end) (12). A cross-sectional 2D model created from XZ plane. Intersecting point of the proximal and distal axis defined as point C, proximal and distal points were defined point A and point B respectively. The angle between these axes was defined as femoral bowing angle (FBA) 9.33° shown in Figure 1b.Two groups of different types of femur models are created. In the first group, straight stems with three different lengths were modelled as seen in Figure 2a, Figure 2b.



Figure 1a. CT coronal view,

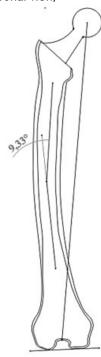


Figure 1b. Femoral bowing angle measurement in coronal plane

All models were designed manually with reference to the geometry of stem in our patient's CT data, which was considered as the middle length straight stem model. In the first model, stem ended proximal to the point C, intersection of two femoral axes, and stem longitudinal axis remained same with CT-data. In the second model, stem geometry remained same and ended nearly on point C. In the last model, stem was positioned in the cancellous bone, distal to point C, so that penetration into cortical bone was minimal. In the second group, two anatomical shaped implants with two different sizes were used. Stem geometries of these implants were created using femoral shaft curvature created with three points in Figure 3a and Figure 3b. In all models, femoral offset distance remained same for an accurate assessment.

# **Mesh and Boundary Conditions**

All femur and implant geometries meshed with second order tetrahedral elements with a global element size of 3 mm were used for the FE models. All contact surfaces were accepted fully bonded. Distal faces of lateral and medial condyle were fixed in all displacement. For boundary condition, static loads were applied to the FE models, which was based on the study by Heller et al. (13,14), consist of the hip contact load and a set of simplified muscle forces (abductor, vastus lateralis, and vastus medialis), and the distal end of the femur was fully fixed as shown in Figure 4.



Figure 2a. Frontal views of straight stem models,



Figure 2b. Sagittal views of straight stem models



Figure 3a. Frontal views of anatomic stem models



Figure 3b. Sagittal views of anatomic stem models

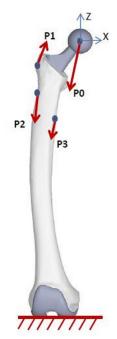


Figure 4. Boundary conditions and material properties

The hip contact and muscle forces were applied as a percentage of the body weight (%BW) to simulate the peak load during stair climbing, which is the most critical load affecting the stability of the femoral stem among all daily activities. All material settings were based on literature values (Table I).

Table I. Young modulus and Poisson ratio values according to material properties				
Force (%body weight)	X	у	z	point
Hip contact	-72.3	-88.6	-333.4	P0
Abductor	83	35.6	77.3	P1
Vastus lat	-2.2	22.4	-135.1	P2
Vastus med	-8.8	39.6	-26.7	P3
	Young Modulus		Poisson Ratio	
Cortical bone	18		0.33	
Trabecular	1		0.2	
Ti-6AI-4V	113.8		0.33	
Knee Component	210		0.33	

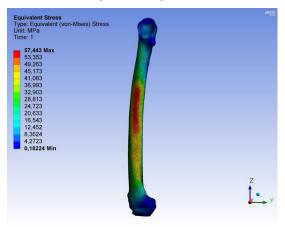
Cortical and trabecular bone geometries of orthotropic materials were used. Young's modulus and Poisson's ratio were taken to be 1000 N/mm2 and 0.2 for the trabecular bone, and 18,000 N/mm2 and 0.3 for the cortical bone

in axial (Z) direction (15) and for other directions young modulus and all shear modulus and Poisson ratios were calculated from equations (16). All finite element analysis are static and solved in ANSYS Workbench.

Von mises stresses concentrations in straight and anatomical stem models are given in figure 5a, 5b, 5c and figures 6a, 6b respectively Maximum von mises stresses for the short straight stem are concentrated over the area between the apex of lateral femoral curvature and the tip of the stem (Point C).

Likewise, for the middle straight stem, stresses are maximum on the narrow area between the tip and apex. Whereas in the long straight stem model maximum stress value decreased and concentration area shifted distally. Compared to the middle straight stem model, middle anatomic stem showed a lower maximum stress value, with a similar stress distribution pattern. However, the long anatomic stem did not lead to stress concentrations on any area of the femur and a uniform stress distribution was obtained. Besides maximum von Mises stresses for the long anatomical stem was found to be lower than any other model.

Principle stress concentrations on the lateral side of the femur for each model are given in Figure 7a-e. Maximum principle stresses on lateral mid-shaft, where two axes intersect (Point C) are given in Figure 8.



**Figure 5.** Von Mises stresses concentrations in straight stem models, **a.** Short

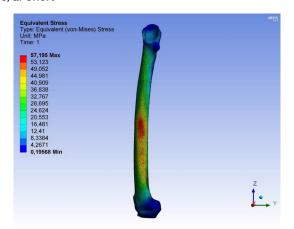


Figure 5b. medium and

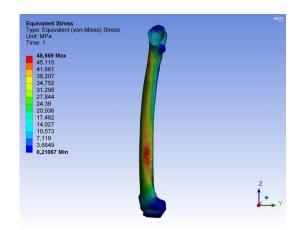


Figure 5c. long respectively

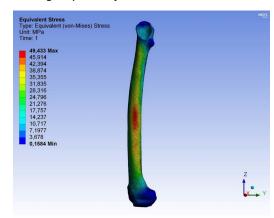


Figure 6a. Max von Mises stresses on anatomical shaped implants aMedium

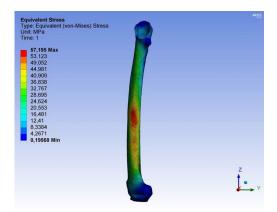


Figure 6b. Long respectively

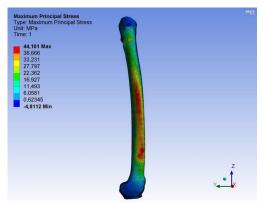


Figure 7. Principle stress concentrations on lateral side a. short

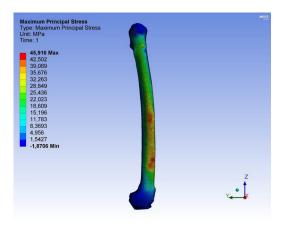


Figure 7b. Medium

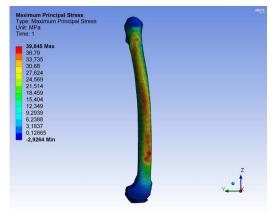


Figure 7c. Long straight stem

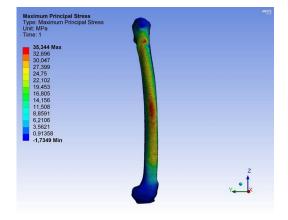


Figure 7d. Anatomic medium size e. anatomic long size

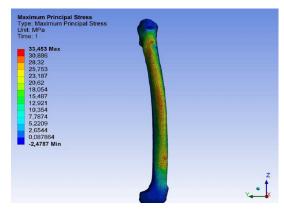


Figure 7e. Anatomic long size

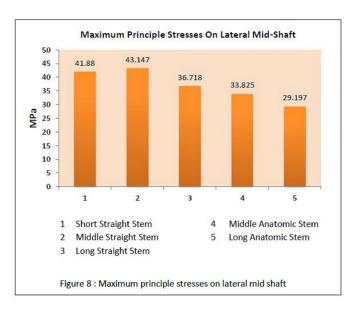


Figure 8. Maximum principle stresses on lateral mid shaft

## DISCUSSION

The most important finding of this study was that the longer femoral stem with lateral bowing provided a uniform stress distribution over the femoral shaft. Also this longer anatomical stem model achieved lower stress concentration values compared to straight models at the same length.

The geometry, size and the material properties of the prosthesis along with technique and extent of fixation have been recognized as important factors which affect the pattern of stress transferred to the femur; determining the stress shielding over the bone. Stress transfer to the femur is beneficial as it ensures a stimulus for maintaining bone mass and protects the bone against disuse osteoporosis. It has been known that a precise fit of the femoral stem in the femur minimizes stress shielding and the beneficial effects of custom-made implants which provide a precise fit, has been emphasized in the literature. (7,17) Corresponding to the literature, in our study we also observed that the model that most fits to the bowed femur, ensured minimum stress values.

In the quest to establish the optimum length of the femoral stem, the geometry and size of the patient's femoral canal come forward as the most determining two factors. Currently, stems with lengths of varying from 120 to 150 mm are routinely used (18). With the results achieved in this study, longer stems seem to more suitable and safer for bowed femurs. On the other hand longer stems reaching to the isthmus have disadvantages such as technically harder placing with a tendency towards varus malposition, putting the anterior femoral cortex into risk of perforation due to anterior femoral bowing and insufficient cementing beyond the isthmus. However, in cases of fractured or weakened femoral cortex especially in revision surgery, longer stems are essential.

The femoral structure and morphology vary widely among different ages and sexes. Lateral bowing is one of these

morphologic variances of the femur especially seen in elderly females from Asian race (9). These variations in femur morphology increase with age, as well as the incidence of proximal femoral fractures. On the other hand, most prosthesis currently used (including the straight femoral stem used in our study) are designed based on the normal femoral structure, neglecting the age-dependent variations. Changes of both bone structure (osteoporosis) and lower extremity biomechanics in elder patients are considered to cause alteration of stress distribution, which may lead to periprosthetic fractures around the femoral stem. Due to the increased comorbidities of elder patients such as diabetes, hypertension, heart failure, etc. multiple revision surgeries could lead to extra costs in addition to morbidity. Considering the life-threatening outcomes of revision surgeries, every effort should be made to refrain from this intricacy (6). With this point of view; the potentially higher costs of custom made prosthesis that fits to bowed femurs should be embraced, in order to avoid any kind of secondary interventions.

In addition to the increase in life expectancy, the number of younger patients undergoing hip replacement is also rising. With the potential risk of trauma and infection, revision surgeries are expected to increase consequently. Surgeons may consider short femoral components as safer options in hip replacement; however it is not clearly proven whether shorter femoral stems provide better outcomes or easier revision surgeries (19). The decision making process for the specific length of femoral stem should include; optimal stress distribution over the proximal femur; and maximum bone preservation combined with optimum stability. While opting for the most suitable femoral component type; surgeons should keep in my mind that depending on the variable patient specific factors such as femoral morphology or bone mineral density; different femoral stems with varying lengths and designs may provide the optimum long lasting outcomes (19).

There are some major limitations of our study which includes the lack of comparison of our deformity model with a normal shaped femur model. Also our model was created using CT data of only one patient with lateral bowing deformity. Further clinical and biomechanical studies are needed to understand the true prevalence especially in older population of this deformity and its role on periprosthetic fractures. Besides, cemented femoral components are also commonly applied for the elderly osteoporotic patients. Not involving cemented models for comparison to evaluate the different stress distribution and load transfer patterns between cement and bone interface, is also a limitation of the current study. The number of cases in which the existing stems cannot be used, or the prevalence of lateral bowing deformities among our population would be of great value for reflecting findings of our work into the clinic.

## CONCLUSION

In our study, we focused on the stress distribution around

long stemmed femoral prosthesis in patients with lateral femoral bowing deformity which is usually not taken into account despite its remarkable prevalence, especially among older females. Our study revealed that particularly for patients with a lateral bowing deformity longer anatomical femoral stems may overcome the excessive stress shielding arising from shorter stems. In selected cases with lateral femoral bowing deformity, after evaluation of the femoral geometry with CT, application of custom-made longer anatomical femoral stems may provide stress distribution over a wider region of the femur.

Competing interests: The authors declare that they have no competing interest.

Financial Disclosure: There are no financial supports

Ethical approval: As the nature of computer tomography based finite element analysis modelling, no ethical committee or IRB approval was required

Nihat Demirhan Demirkiran ORCID: 0000-0002-0724-9672 Mehmet Erduran ORCID: 0000-0002-0668-7224 Turan Cihan Dulgeroglu ORCID: 0000-0002-9661-5418

# **REFERENCES**

- 1. Wilcock GK. Economic aspects of the demand for total hip replacement in the elderly. Age Ageing 1978;8:32-5.
- Mahomed NN, Barrett JA, Katz JN, et al. Rates and outcomes of primary and revision total hip replacement in the United States Medicare population. J Bone Joint Surg Am 2006:85:27-32.
- Mahomed N, Katz JN. Revision total hip arthroplasty: indications and outcomes. Arthritis Rheum 1996;39:1939-50.
- 4. Della Rocca GJ, Leung KS, Pape HC. Periprosthetic fractures: epidemiology and future projections. J Orthop Trauma 2011;25:66-S70.
- 5. Berry DJ. Epidemiology: hip and knee. Orthop Clin North Am. 1999;30:183-90.
- Franklin J, Henrik M. Risk factors for periprosthetic femoral fracture. Injury 2007;38:655-60.
- Götze C, Steens W, Vieth V, et al. Primary stability in cementless femoral stems:custom-made versus conventional femoral prosthesis. Clin Biomech ((Bristol, Avon) 2002;17:267-73.
- 8. Casper DS, Kim GK, Parvizi J, et al. Morphology of the proximal femur differs widely with age and sex: relevance to design and selection of femoral prostheses. J Orthop Res. 2012;30:1162-6.
- Oh Y, Wakabayashi Y, Kurosa Y, et al. Potential pathogenic mechanism for stress fractures of the bowed femoral shaft in the elderly: mechanical analysis by the CT-based finite element method. Injury 2014;45:1764-71.
- Pieper S, Halle M, Kikinis R, 3D Slicer. Proceedings of the IEEE Symposium on Biomedical Imaging; April 15-18,2004; Arlington, Virginia, USA. p. 632-5.
- 11. Bergmann G, Deuretzbacher G, Heller M, et al. Hip contact forces and gait patterns from routine activities. J Biomech 2001;34:859-71.
- 12. Mullaji AB, Marawar SV, Mittal V. A comparison of coronal plane axial femoral relationships in Asian patients with varus osteoarthritic knees and healthy knees. J Arthroplasty 2009;24:861-7.
- 13. Heller MO, Bergmann G, Kassi JP, et al. Determination of muscle loading at the hip joint for use in pre-clinical testing.

- J Biomech 2005;38:1155-63.
- 14. Heller MO, Bergmann G, Deuretzbacher G, et al. Musculoskeletal loading conditions at the hip during walking and stair climbing. J Biomech 2001;34:883-93.
- Wirtz DC, Schieffers N, Pandorf T, et al. Critical evaluation of known bone material properties to realize anisotropic Fesimulation of the proximal femur. J Biomech 2000;33:1325-30.
- 16. San Antonio T, Ciaccia M, Müller-Karger C, et al. Orientation of orthotropic material properties in a femur FE model: a
- method based on the principal stresses directions. Med Eng Phy 2012;34:914-9.
- 17. Bieger R, Ignatius A, Decking R, et al. Primary stability and strain distribution of cementless hip stems as a function of implant design. Clin Biomech (Bristol, Avon) 2012;27:158-64.
- Korkmaz MF, Sevimli R. Total Hip Artroplasty. J Clin Anal Med 2015;6:
- Feyen H, Shimmin AJ. Is the length of the femoral component important in primary total hip replacement? Bone Joint J 2014:96:442-8.